

# A compressible two-layer mixed-flow model.

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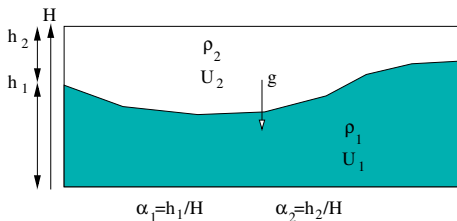
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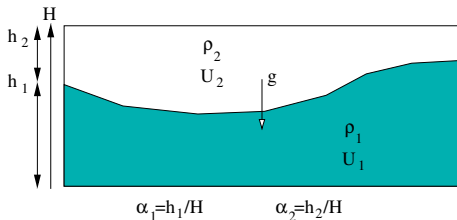
The Compressible Two-Layer (CTL) model [1,2] has been proposed in order to model liquid/gas flows in pipes with the following features:

- uniform diameter of the pipes;
- one velocity for each phase (possibility of counter-current flows);
- compressibility of the phases;
- thermal aspects where first out of the scope of the targetted applications (barotropic EOS, no equation for energies);
- stratification due to gravity (liquid is below the gas);
- **initially without mass transfer.**



[1] *A compressible two-layer model for transient gas-liquid flows in pipes*, C. Demay, J.-M. Hérard, CMAT, 2017.

[2] *Modélisation et simulation d'écoulements transitoires diphasiques eau-air dans les circuits hydrauliques*, C. Demay, PhD Thesis, 2017.



Barotropic Baer-Nunziato like model:

$$\left\{ \begin{array}{l} \frac{\partial}{\partial t} (\alpha_2) + \frac{Q_2}{m_2} \frac{\partial}{\partial x} (\alpha_2) = \Phi_2 = -\Phi_1, \\ \frac{\partial}{\partial t} (m_1) + \frac{\partial}{\partial x} (Q_1) = M_1, \\ \frac{\partial}{\partial t} (Q_1) + \frac{\partial}{\partial x} (Q_1^2/m_1 + \alpha_1 P_1(\alpha_1/m_1)) + \mathcal{P}_I(\alpha_1, m_1) \frac{\partial}{\partial x} (\alpha_2) = \bar{V} M_1 - \lambda_u (U_1 - U_2), \\ \frac{\partial}{\partial t} (m_2) + \frac{\partial}{\partial x} (Q_2) = -M_1, \\ \frac{\partial}{\partial t} (Q_2) + \frac{\partial}{\partial x} (Q_2^2/m_2 + \alpha_2 P_2(\alpha_2/m_2)) - \mathcal{P}_I(\alpha_1, m_1) \frac{\partial}{\partial x} (\alpha_2) = -\bar{V} M_1 + \lambda_u (U_1 - U_2), \end{array} \right.$$

with:  $\alpha_1 + \alpha_2 = 1$ ,  $m_k = \alpha_k \rho_k$ ,  $Q_k = m_k U_k$ ,  $\bar{V} = (U_1 + U_2)/2$  and where  $\tau_k \rightarrow P_k(\tau_k)$  are EOS specified by the user. Interfacial pressure reads:

$$\mathcal{P}_I = P_1(\tau_1) - \frac{g \alpha_1 H \rho_1}{2}.$$

Closure of the source terms thanks to a convex energy (counterpart of entropic criterion for BN model with energy):

$$E = E_1 + E_1^p + E_2, \quad \text{with } E_k = m_k(e_k + U_k^2/2) \quad \text{and } E_1^p = \alpha_1 m_1 gH/2.$$

This leads to:

$$\frac{\partial}{\partial t} (E) + \frac{\partial}{\partial x} (U_1(E_1 + E_1^p + \alpha_1 P_1) + U_2(E_2 + \alpha_2 P_2)) = \left( h_1 + \frac{\alpha_1 gH}{2} - h_2 \right) M_1 + (P_2 - \mathcal{P}_I) \Phi_1 - \lambda_u (U_1 - U_2)^2,$$

with  $h_k = e_k + P_k \tau_k$  and  $\lambda_u \geq 0$ . Classical choices are possible for  $M_1$  and  $\Phi_1$ , i.e.:

$$M_1 = -\lambda_m \left( h_1 + \frac{\alpha_1 gH}{2} - h_2 \right), \quad \text{and } \Phi_1 = -\lambda_p (P_2 - \mathcal{P}_I), \quad \text{with } \lambda_m, \lambda_p \geq 0.$$

**But, an other choice is proposed on the basis of [3].** The following energy is defined:

$$(\alpha_1, m_1) \mapsto \mathcal{E}_0^\#(\alpha_1, m_1) = m_1 e_1 \left( \frac{\alpha_1}{m_1} \right) + \alpha_1 m_1 \frac{gH}{2} + (m^0 - m_1) e_2 \left( \frac{1 - \alpha_1}{m^0 - m_1} \right),$$

with  $m_0 = m_1 + m_2$ .

It can be proved that it is strictly convex provided that the following sufficient condition is fulfilled:

$$\frac{1}{2} \sqrt{gH} < \min(c_1, c_2),$$

i.e. speed of gravity waves < speed of sound in pure phases. We assume that this condition holds in the following.

[3] *Various choices of source terms for a class of two-fluid two-velocity models*, O. Hurisse, ESAIM: M2AN, 2021.

We have:

$$\frac{\partial}{\partial \alpha_1} (\mathcal{E}_0^\#) = P_2 - \mathcal{P}_1, \quad \text{and} \quad \frac{\partial}{\partial m_1} (\mathcal{E}_0^\#) = h_1 - h_2 + \frac{\alpha_1 g H}{2},$$

so that:

$$\begin{aligned} & \frac{\partial}{\partial t} (E) + \frac{\partial}{\partial x} (U_1(E_1 + E_1^p + \alpha_1 P_1) + U_2(E_2 + \alpha_2 P_2)) \\ &= \frac{\partial}{\partial m_1} (\mathcal{E}_0^\#) M_1 + \frac{\partial}{\partial \alpha_1} (\mathcal{E}_0^\#) \Phi_1 - \lambda_u (U_1 - U_2)^2 \\ &= \nabla_{(\alpha_1, m_1)} \mathcal{E}_0^\# (\alpha_1, m_1) \cdot \begin{pmatrix} \Phi_1 \\ M_1 \end{pmatrix} - \lambda_u (U_1 - U_2)^2. \end{aligned}$$

Since  $\mathcal{E}_0^\#$  is strictly convex wrt.  $(\alpha_1, m_1)$ , there exists a unique minimizer  $(\bar{\alpha}_1, \bar{m}_1)$  so that:

$$0 \geq \mathcal{E}_0^\# (\bar{\alpha}_1, \bar{m}_1) - \mathcal{E}_0^\# (\alpha_1, m_1) \geq \nabla_{(\alpha_1, m_1)} \mathcal{E}_0^\# (\alpha_1, m_1) \cdot \begin{pmatrix} \bar{\alpha}_1 - \alpha_1 \\ \bar{m}_1 - m_1 \end{pmatrix}.$$

Hence, by choosing:

$$M_1 = \lambda (\bar{m}_1 - m_1) \quad \text{and} \quad \Phi_1 = \lambda (\bar{\alpha}_1 - \alpha_1),$$

with the same  $\lambda$  for both source terms and  $\lambda \geq 0$ , we get:

$$\frac{\partial}{\partial t} (E) + \frac{\partial}{\partial x} (U_1(E_1 + E_1^p + \alpha_1 P_1) + U_2(E_2 + \alpha_2 P_2)) \leq 0$$

- Extension of the CTL model [1,2] to flows with mass transfer.
- Homogeneous-like “BGK” source terms for two-fluid models (extension to BN model with energy, see [3]).
- Thermodynamical disequilibrium source terms are written in a more linear form wrt. primal variables.
- In a numerical point of view, treatment of these terms is more easy.
- Coupling of convection terms and source terms is more easy, see [4] for an example while using a MAC/SIMPLE fractional step scheme.

[1] *A compressible two-layer model for transient gas–liquid flows in pipes*, C. Demay, J.-M. Hérard, CMAT, 2017.

[2] *Modélisation et simulation d'écoulements transitoires diphasiques eau-air dans les circuits hydrauliques*, C. Demay, PhD Thesis, 2017.

[3] *Various choices of source terms for a class of two-fluid two-velocity models*, O. Hurisse, ESAIM: M2AN, 2021.

[4] *A semi-implicit fractional step algorithm on staggered meshes for simulating a compressible two-layer mixed-flows model*, O. Hurisse, submitted.