# A continuous-time optimal control approach based on Pontryagin's Maximum Principle with chance constraints

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# Summary

- 1 Introduction: continuous-time optimal control with chance constraints
- Writing the optimal control problem
- Writing the Hamiltonian and the ODE system
- Problem formulation
- 5 Application to reference trajectory planning problem
- 6 Conclusion

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# Introduction









#### Introduction

- Continuous-time optimal control with chance constraints to handle uncertainty
- ullet Chance constraints guarantee a threshold of performance lpha of satisfaction
- We can derive a deterministic equivalent formulation in SOCP (second-order conic programming) [Van de Panne and Popp, 1963]
- Comparison:
  - Solving the optimal control problem as a nonlinear optimisation problem with integral cost function [Valli et al., 2025]
  - Solving an ODE system as a two-point boundary value problem
- Application to reference trajectory planning generation for autonomous vehicles











# Writing the optimal control problem











# Problem setup

- Let  $n, m \in \mathbb{N}$  be dimensions of state and control vectors respectively  $z(t) \in \mathbb{R}^n$ ,  $u(t) \in \mathbb{R}^m$ . Let  $t_i \in \mathbb{R}$ ,  $t_i \ge 0$  the final time.
- Integrand  $I: \mathbb{R}^n \times \mathbb{R}^m \longmapsto \mathbb{R}$ , Integral cost function  $J: \mathbb{R}^m \mapsto \mathbb{R}$ , Controls  $\mathbf{u} = (u(t))_{t \in [0,t_f]}$  and states  $\mathbf{z} = (z(t))_{t \in [0,t_f]}$

#### Cost function

$$J(\mathbf{u}) = \int_0^{t_f} I(z(t), u(t)) dt$$
 (1)











# Optimisation problem

- Let  $\alpha \in [0, 1]$
- Control-state equation:  $f : \mathbb{R}^n \times \mathbb{R}^m \mapsto \mathbb{R}^n$ ,
- Random vector  $a \sim \mathcal{N}(\mu, \Sigma)$ , with  $\mu \in \mathbb{R}^n$  the mean vector and  $\Sigma \in \mathbb{R}^{n \times n}$  the covariance matrix,  $b \in \mathbb{R}$

# Optimisation problem with chance constraint

$$\min_{\mathbf{u}} J(\mathbf{u})$$
s.t. 
$$\frac{dz(t)}{dt} = f(z(t), u(t))$$

$$\mathbb{P}(a^{\mathsf{T}}z(t) \le b) \ge \alpha$$











(2)

#### Chance constraint reformulation

 Thanks to [Van de Panne and Popp, 1963], the chance constraint is equivalent to a second-order conic programming (SOCP) constraint

#### Chance constraint

$$\mathbb{P}(\boldsymbol{a}^{\mathsf{T}}\boldsymbol{z}(t) \leq \boldsymbol{b}) \geq \alpha \Longleftrightarrow \mu^{\mathsf{T}}\boldsymbol{z}(t) + \boldsymbol{F}^{-1}(\alpha) \|\boldsymbol{\Sigma}^{1/2}\boldsymbol{z}(t)\|^{2} \leq \boldsymbol{b}$$
 (3)

#### with

- $F(\cdot)$  the cumulative distribution function (CDF) of the standard normal distribution  $\mathcal{N}(0,1)$ .
- || ⋅ || the Euclidean norm











# Writing the Hamiltonian









# Path constrained optimisation problems for nonlinear dynamic systems

From [Bryson, 2018], chapter 3.11, let

#### Constraint on function of the state variable

$$S(z(t)) := \mu^{T} z(t) + F^{-1}(\alpha) z(t)^{T} \Sigma z(t) - b$$
 (4)

Inequality constraint on function of the state variables only  $S(z(t)) \le 0$ 

#### Let

- $\lambda(t) \in \mathbb{R}^n$  the costates associated to z(t)
- $\eta(t) \in \mathbb{R}^n$ ,  $\eta(t) \ge 0$  the time-dependent Lagrangian multipliers associated to S(z(t))











# Time-dependent Lagrangian multipliers

• Time-dependent Lagrangian multipliers  $\eta(t)$  are defined such as

# Time-dependent Lagrangian multipliers

$$\begin{cases} \eta(t) = 0 & \text{if } S(z(t)) < 0 \\ \eta(t) > 0 & \text{if } S(z(t)) = 0 \end{cases}$$

$$(5)$$

#### Remark

Depending on the problem studied, discontinuities may appear at constraint saturation, leading to singular arcs [Bryson, 2018]











# q-th order state variable inequality constraint

- To control the system at constraint saturation S(z(t)) = 0, we need to find  $q \in \mathbb{N}$  as the q th time derivative of the constraint S(z(t)) depends explicitly on the command u(t).
- The order q is fixed such as it exists  $g : \mathbb{R}^n \times \mathbb{R}^m \longmapsto \mathbb{R}^n$  verifying the following condition:

#### q-th order state variable inequality constraint

$$\frac{d^{(q)}S(z(t))}{dt^{(q)}} = g(z(t), u(t))$$
 (6)











# Tangency conditions

ullet The following condition must be checked for the command u(t) to be optimal

#### Tangency conditions

$$\frac{d^{(q)}S(z(t))}{dt^{(q)}} = 0 \quad \text{if } S(z(t)) = 0 \tag{7}$$











#### Hamiltonian formulation

The Hamiltonian writes as

#### Hamiltonian

$$H(z(t), u(t), \lambda(t), \eta(t)) = I(z(t), u(t)) + \lambda^{T}(t) \cdot f(z(t), u(t))$$

$$+ \eta^{T}(t) \cdot \frac{d^{(q)}S(z(t))}{dt^{(q)}}$$
(8)











# Problem formulation











# **Euler-Lagrange equations**

• The Euler-Lagrange equations give ordinary differential equations to determine the costates  $\lambda(t)$ 

## Euler-Lagrange equations for costates $\lambda(t)$

$$\frac{d\lambda(t)}{dt} = -\frac{\partial H(z(t), u(t), \lambda(t), \eta(t))}{\partial z(t)} \tag{9}$$











# Transversality conditions and optimal command

In our problem, there is no constraint at final time, therefore

$$\lambda(t_f) = 0 \tag{10}$$

• The optimal command  $u^*(t)$  is obtained by

### Optimal command $u^*(t)$

$$u^{*}(t) = \operatorname{argmin}_{u_{\min} \le u(t) \le u_{\max}} H\left(z(t), u(t), \lambda(t), \eta(t)\right)$$
(11)

It verifies the condition

$$\frac{\partial H(z(t), u^*(t), \lambda(t), \eta(t))}{\partial u(t)} = 0 \tag{12}$$











# Two-Point Boundary Value Problem (TPBVP)

Finally, we obtain the two-point boundary value problem such as

#### TPBVP schema

$$\frac{z(0)}{\lambda(0)?} \begin{cases}
\frac{dz(t)}{dt} = f(z(t), u(t)) \\
\frac{d\lambda(t)}{dt} = -\frac{\partial H(z(t), u(t), \lambda(t), \eta(t))}{\partial z(t)}
\end{cases}$$

$$\frac{z(t_f)}{\lambda(t_f) = 0}$$
(13)











# $\lambda^*(0)$ and shooting method

Therefore, the control is determined by optimal initial values

#### Optimal initial values $\lambda^*(0)$

$$\lambda^*(0) = \operatorname{argmin}_{\lambda(0)} \|\lambda(t_f)\| \tag{14}$$

- Classical approach to solve this problem is to use the shooting method [Morrison et al., 1962]
- In our application, we use Levenberg-Marquardt algorithm [Gavin, 2019] with an estimation  $\tilde{\lambda}(0)$  as starting point, obtained by reversing the system (13) using results of our previous work [Valli et al., 2025] with costates  $\lambda(t_f) = 0$ . We use GEKKO optimisation solver [Beal et al., 2018].











# Resolution steps

#### **Algorithm** Solving the continuous-time optimal control problem

- 1: **Initialize** z(0) initial state,  $t_f$  final time
- 2: **Solve** the optimal control problem using GEKKO solver starting from initial state z(0)
- return  $(z^{GEKKO}(t), u^{GEKKO}(t))_{[0,t_f]}$
- **Reverse integration** of the TPBVP starting from  $(z^{GEKKO}(t_f), \lambda(t_f) = 0)$
- return  $(\tilde{z}(0), \tilde{\lambda}(0))$
- 6: Optimise the initial costates by Levenberg-Marguardt algorithm applied on the TPBVP starting from  $(z(0), \tilde{\lambda}(0))$
- return  $\lambda^*(0)$
- **Forward integration** of the TPBVP
- **return**  $(z^{Pontryagin}(t), u^{Pontryagin}(t))_{[0,t_f]}$











# Application to trajectory planning problem











# Trajectory planning I

 We represent the vehicle controlled (the ego vehicle) by its Cartesian coordinates.

# Command u(t) and state z(t)

$$u(t) = \begin{pmatrix} j_t \\ \omega_t \end{pmatrix} \qquad (15) \qquad \qquad z(t) = \begin{pmatrix} x_t \\ y_t \\ \theta_t \\ v_t \\ a_t \end{pmatrix} \qquad (16)$$

- $j_t$  is the jerk,  $\omega_t$  the angular velocity
- $(x_t, y_t)$  the Cartesian coordinates,  $\theta_t$  the heading angle of the ego vehicle,  $v_t$  the linear speed and  $a_t$  the linear acceleration











# Trajectory planning II

• The control-state relationship is given by :

#### Control-state equation

$$\frac{dz(t)}{dt} = f(z(t), u(t)) = \begin{pmatrix} v_t \cos(\theta_t) \\ v_t \sin(\theta_t) \\ \omega_t \\ a_t \\ j_t \end{pmatrix}$$
(17)











# Objective function

• The waypoints  $(x_t^{wp}, y_t^{wp}, \theta_t^{wp})_{t>0}$  corresponds to the centre lane of the road,  $v_r$  the recommended linear speed

### Objective function

$$\int_{0}^{t_{f}} \mathbf{w'}_{x}(t) \left(\frac{x_{t}}{x_{t}^{wp}} - 1\right)^{2} + \mathbf{w'}_{y}(t) \left(\frac{y_{t}}{y_{t}^{wp}} - 1\right)^{2} + \mathbf{w'}_{h}(t) \left(\frac{\theta_{t}}{\theta_{t}^{wp}} - 1\right)^{2}$$

$$+ \mathbf{w'}_{v} \left(\frac{v_{t}}{v_{r}} - 1\right)^{2} + \mathbf{w'}_{a} \cdot a_{t}^{2} + \mathbf{w'}_{\omega} \cdot \omega_{t}^{2} + \mathbf{w'}_{j} \cdot j_{t}^{2}$$

$$+ \mathbf{w}_{p} \cdot P(x_{t}^{tgt}, y_{t}^{tgt}, x_{t}, y_{t}) dt$$

$$(18)$$











# Adaptive Cruise Control (ACC) feature

The ACC feature [Liu et al., 2017] is modelled by

### Adaptive Cruise Control

$$P(x_t^{tgt}, y_t^{tgt}, x_t, y_t) = \frac{1}{e^{-\left(\frac{(x_t^{tgt} - x_t)^2 + (y_t^{tgt} - y_t)^2}{2}\right)\left(1 + \operatorname{erf}\left(\frac{\operatorname{sign}(x_t^{tgt} - x_t)\sqrt{(x_t^{tgt} - x_t)^2 + (y_t^{tgt} - y_t)^2}}{\sqrt{2}}\right)\right)}$$

With

$$\forall x \in \mathbb{R} \quad \operatorname{erf}(x) = \frac{2}{\sqrt{\pi}} \int_0^x e^{-t^2} dt$$
 (20)











# Chance constraints on target distance

Uncertainty on target vehicle position:

$$\mathbf{x}_{t}^{tgt} \sim \mathcal{N}(\mu_{\mathbf{x}_{t}}, \sigma_{\mathbf{x}_{t}}), \mathbf{y}_{t}^{tgt} \sim \mathcal{N}(\mu_{\mathbf{y}_{t}}, \sigma_{\mathbf{y}_{t}})$$
 (21)

#### Deterministic constraints

From [Valli et al., 2025]

$$\mathbb{P}(|x_t - x_t^{tgt} + y_t - y_t^{tgt}| \ge d_{min}) \ge \alpha \Longrightarrow$$
 (22)

$$x_t + y_t \le \mu_{x_t} + \mu_{y_t} + d_{min} + \sqrt{\sigma_{x_t}^2 + \sigma_{y_t}^2} F_N^{-1} \left(\frac{\alpha}{2}\right)$$
 (23)

$$x_t + y_t \ge \mu_{x_t} + \mu_{y_t} - d_{min} + \sqrt{\sigma_{x_t}^2 + \sigma_{y_t}^2} F_N^{-1} \left( 1 - \frac{\alpha}{2} \right)$$
 (24)











# Experiments setup

Parameter	Function	Value
V <sub>r</sub>	Reference linear speed	12 m.s <sup>-1</sup>
d <sub>min</sub>	Minimum distance between vehicles	5 m
v <sub>max</sub>	Maximum linear speed	40 m.s <sup>-1</sup>
$\omega_{max}$	Maximum angular speed	$\frac{\pi}{6} s^{-1}$
a <sub>max</sub>	Maximum acceleration	2 m.s <sup>-2</sup>
j <sub>max</sub>	Maximum jerk	$0.6 \; m.s^{-3}$

Table: Parameters' values for urban driving scenarios during the simulation.



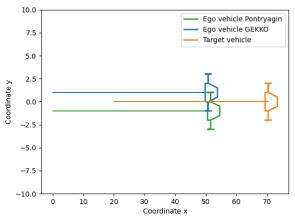








# Trajectory comparison







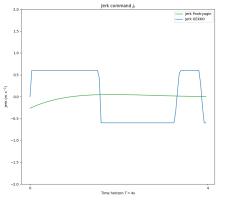


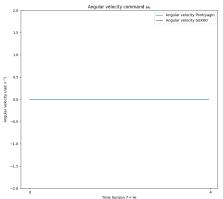




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# **Optimal Commands**









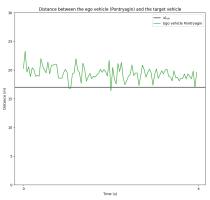


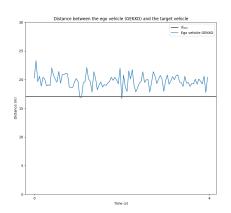




#### Constraint violations

#### Distance between vehicles













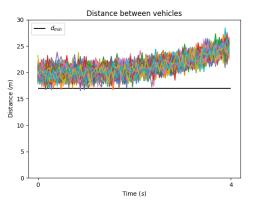


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# Out-of-sample analysis

Apply the control  $u^*(t)$  to other realisations  $x_t^{tgt} \sim \mathcal{N}(\mu_{x_t}, \sigma_{x_t})$ ,  $y_t^{tgt} \sim \mathcal{N}(\mu_{y_t}, \sigma_{y_t})$ 













#### Conclusion

- Pontryagin solver achieves smoother command than approximated bang-bang control obtained by direct methods
- It better minimise the cost function, but finding initial conditions can be cumbersome
- Further perspectives: study the impact of approximations in the model (choice for derivative of sign(·), ODE solver and optimisation technique); extend to higher time horizons; apply to other optimal control problems











# Thank you!









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Pontryagin with chance constraints











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# Appendices













# Appendix I: Transversality conditions

- Transversality conditions on the costates  $\lambda(t_f)$  depend on the constraints at final time  $t_f$ .
- Let  $\Psi : \mathbb{R}^n \longmapsto \mathbb{R}^n$  represents the equality constraints on the final state such as  $\Psi(z(t_f)) = 0$  and  $\nu \in \mathbb{R}^n$  the Lagrange multipliers associated.
- Let  $\Phi(t_f) \in \mathbb{R}$  the terminal cost function such that

$$J(\mathbf{u}) = \int_0^{t_f} I(z(t), u(t)) dt + \Phi(t_f)$$
 (25)

#### Transversality conditions

$$\lambda(t_f) = \frac{\partial}{\partial z(t_f)} (\Phi(t_f) + \nu^T \Psi(t_f))$$
 (26)











# Appendix II: Numerical simulation I

- Time horizon: T = 4 s, time step  $\Delta t = 0.04 s$
- Driving along the road, straight line  $(\forall t \in \mathbb{R}^+ \ y_t = 0, \theta_t = 0)$

#### **GEKKO Solving**

$$z(0) = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 13.038 \\ 0 \end{pmatrix} \qquad (27) \qquad z^{GEKKO}(t_f) = \begin{pmatrix} 50.81 \\ 0 \\ 0 \\ 12.61 \\ 0.01 \end{pmatrix} \qquad (28)$$

$$e^{GEKKO}(t_f) = \begin{bmatrix} 0 \\ 0 \\ 12.61 \end{bmatrix}$$









# Appendix II: Numerical simulation II

#### Reverse integration

$$\tilde{z}(0) = \begin{pmatrix}
-1.662 \\
0 \\
0 \\
14.840 \\
-1.631
\end{pmatrix}$$
(29)
$$\tilde{\lambda}(0) = \begin{pmatrix}
-4.546 \\
0 \\
0 \\
-8.242 \\
-16.277
\end{pmatrix}$$
(30)











# Appendix II: Numerical simulation III

#### Levenberg-Marguardt optimisation

$$\lambda^*(0) = \begin{pmatrix} 0.572 \\ -9.194 * 10^{-17} \\ 1.460 * 10^{-16} \\ 0.959 \\ 0.533 \end{pmatrix}$$
 (31)











# Appendix III: Optimal cost

Numerical integration using Simpson's method

## Optimal cost for GEKKO solver

$$J_{GEKKO}^*: \int_0^{t_f} I(z^{GEKKO}(t), u^{GEKKO}(t)) dt = 8.90$$
 (32)

#### Optimal cost for Pontryagin solver

$$J_{Pontryagin}^*: \int_0^{t_f} I(z^{Pontryagin}(t), u^{Pontryagin}(t)) dt = 4.91$$
 (33)











# Appendix IV: Energy consumption

Numerical integration using Simpson's method

# Energy for GEKKO solver

$$\int_0^{t_f} ||u^{GEKKO}(t)||_2 dt = 2.32 \tag{34}$$

#### Energy for Pontryagin solver

$$\int_{0}^{t_{f}} ||u^{Pontryagin}(t)||_{2} dt = 0.19$$
 (35)









